# THAMES RIVER BASIN EASTFORD, CONNECTICUT

HALLS POND DAM

CT 00388

AND

CT 00598

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PHASE I INSPECTION REPORT

NATIONAL DAM INSPECTION PROGRAM

SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered)

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Thames River Basin Eastford, Connecticut

20. ABSTRACT (Continue on reverse side if necessary and identity by block number)

Halls Pond Dam includes two dams, with the northerly dam including the spillway and outlet works. The southerly dam consists of a dike only, with no outlet. The north dam is 250 feet long with the original dam being earth fill with masonry faces. This dam has a maximum height of 23.5 feet and a spillway consisting of twin 9' x 3.3' box culberts. The south dam is a 250 foot long earth dike with a maximum height of 14 feet. Halls Pond Dam is classified as SMALL in size with a hazard classification of LOW. The dam is in fair condition with some seepage at the south dam.

# NATIONAL DAM INSPECTION PROGRAM PHASE I INSPECTION REPORT

Identification No.:

CT 00388

CT 00598

Name of Dam:

Halls Pond Dam

Town:

Eastford

County and State:

Windham, Connecticut

Stream:

Slovik Brook

Date of Inspection:

27 February, 1981

#### BRIEF ASSESSMENT

Halls Pond includes two dams, with the northerly dam including the spillway and outlet works. The southerly dam consists of a dike only, with no outlet. Both dams were rebuilt in 1968. This is a State of Connecticut owned pond used for recreation.

The north dam is 250 feet long with the original dam being earth fill with masonry faces. In 1968, an impervious core and pervious shell were added to the downstream face. This dam has a maximum height of 23.5 feet and a spillway consisting of twin 9' x 3.3'box culverts.

The south dam is a 250 foot long earth dike with a maximum height of 14 feet. In 1968, an impervious core with pervious shell was added to the downstream face.

Halls Pond is classified as SMALL in size with a hazard classification

of LOW. The dam is in fair condition with some seepage at the south

dam.

Corps of Engineers Guidelines recommend a test flood of from 50 to 100

year frequency for dams of this size and hazard classification. A 100 year

storm was used with a peak inflow of 560 cfs and a peak outflow of

243 cfs. The spillway will pass this flow with a water surface elevation

of 516.7 without the outlet works operating and elevation 516.3 with the

outlet gate full open.

It is recommended that an engineer study the seepage at the south dam

and that the owner perform any corrective measures required. This

should be done within one year, and the remedial measures detailed in

Section 7 should be accomplished within one year.

FUSS & O'NEILL, INC.

By:

Walter S. Fuss, P.E.

President

#### PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I investigations. Copies of
these guidelines may be obtained from the Office of Chief of Engineers,
Washington, D.C. 20314. The purpose of a Phase I Investigation is to
identify expeditiously those dams which may pose hazards to human life or
property. The assessment of the general condition of the dam is based upon
available data and visual inspections. Detailed investigation, and analyses
involving topographic mapping, subsurface investigations, testing, and detailed
computational evaluations are beyond the scope of a Phase I investigation:
however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the

dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there by any chance that unsafe conditions be detected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonbly possible storm runoff), or fractions thereof. Because of the magnitude and rarity of such a storm event, a finding that a spillway will not pass the test flood should not be interpreted as necessarily posing a highly inadequate condition. The test flood provides a measure of relative spillway capacity and serves as an aide in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

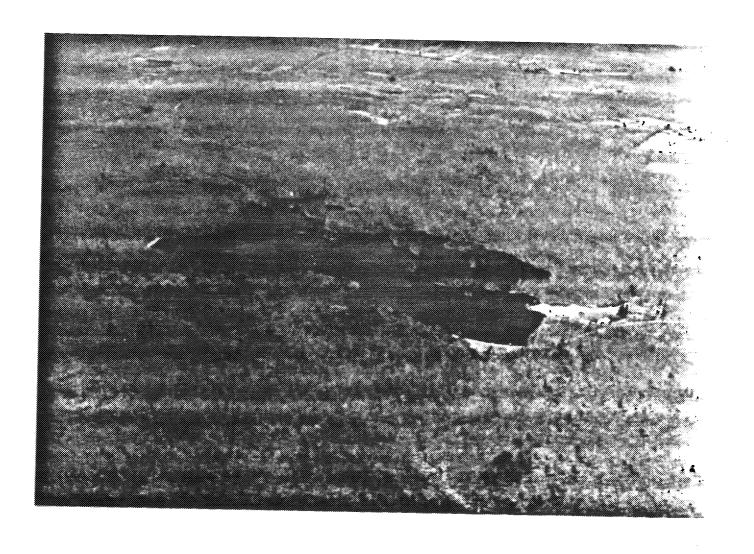
The Phase I Investigation does not include an assessment of the need for fences, gates, no-trepassing signs, repairs to existing fences and railings and other items which may be needed to minimize trespass and provide greater security for the facility and safety to the public. An evaluation of the project for compliance with OSHA rules and regulations is also excluded.

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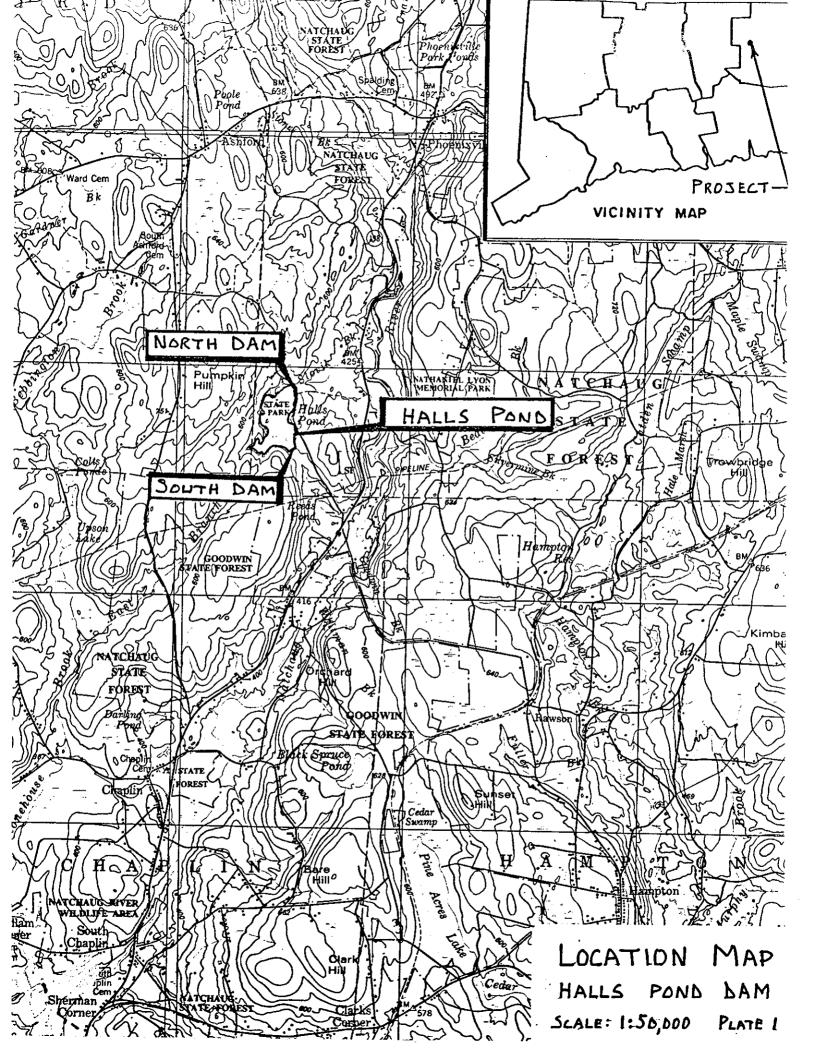
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OVERVIEW PHOTO



# NATIONAL DAM INSPECTION PROGRAM PHASE I INSPECTION REPORT HALLS POND DAM CT 00388 AND 00598

#### SECTION 1 - PROJECT INFORMATION

#### 1.1 GENERAL:

Authority. Public Law 92-367, August 8, 1972, aurhorized the Secretary of the Army, through the Corps of Engineers, to initiate a national program of dam inspection through the United States. The New England Division of the Corps of Engineers has been assigned the responsibility of supervising the inspection of dams within the New England Region. Fuss & O'Neill, Inc. has been retained by the New England Division to inspect and report on selected dams in the State of Connecticut. Authorization and notice to proceed was issued to Fuss & O'Neill, Inc. under a letter of 25 November, 1980 from William E. Hodgson, Jr., Colonel, Corps of Engineers. Contract No. DACW33-81-C-0020 has been assigned by the Corps of Engineers for this work.

#### b. Purpose.

- 1. Perform technical inspection and evaluation of non-federal dams
  to identify conditions which threaten the public safety and thus
  permit correction in a timely manner by non-federal interests.
- 2. Encourage and assist the States to initiate quickly effective dam safety programs for non-federal dams.
- 3. To update, verify and complete the National Inventory of Dams.

#### 1.2 DESCRIPTION

- a. Location. Halls Pond Dam is located in the Town of Eastford,
  County of Windham, on the west side of Kennerson Reservoir Road
  about 0.9 miles northwest of Connecticut Route 198. The north
  dam is at latitude 41°-50.6' and longitude 72°-6.4' and the south
  dam is at latitude 41°-50.2' and longitude 72°-6.5'. Slovik
  Brook starts at Halls Pond Dam and joins the Natchaug River about
  0.8 miles to the east. Natchaug River joins other streams about
  11.5 miles downstream in Willimantic to form the Shetucket River.
  The watershed is rolling and contains 1.3 miles of mostly wooded
  area.
- b. Description of Dam and Appurtenances. There are two dams impounding Halls Pond. The north dam is the main structure and includes outlet works with a gate house and 24 inch outlet pipe as well as a spillway consisting of twin 9 foot by 3.3 foot concrete box culverts. Kennerson Reservoir Road forms the crest of the dam. The north dam is shown in Photos C1-1 through C1-11. An original earth filled masonry faced dam was partially reconstructed in 1968 by adding an impervious core and pervious shell on the downstream slope. This dam has a length of 250 feet.

The south dam is 250 feet long and consists of an original earth dike with an impervious core and pervious shell added in 1968.

There is no outlet at this dam which acts as a dike. The

- crest consists of a 10 foot wide gravel roadway. Photos C2-1 through C2-7 show the south dam.
- c. <u>Size Classification</u>. The north dam has a height of 23.5 feet and the south dam has a height of 14 feet. At top of dam level, the total storage volume is 890 acre-feet. The dam is therefore classified as a SMALL structure in accordance with the recommended guidelines of the Corps of Engineers which defines a small dam as one with a storage capacity of 50 to 1,000 acre-feet and a height of 25 or more but less than 40 feet.
- d. <u>Hazard Classification</u>. This dam is classified as having a LOW hazard potential because no structures would be damaged and only the roadway forming the crest of the north dam would be damaged.
- e. Ownership. Halls Pond Dams are owned by the State of Connecticut and are maintained by the Department of Environmental Protection.
- f. Operator. Operating personnel are under the direction of:

  Region Director

  Department of Environmental Protection
- g. <u>Purpose of Dam</u>. Halls Pond is a recreational lake used mainly for fishing.

- h. Design and Construction History. The design and construction details for the original dam are unknown. Major repairs and reconstruction of both dams were undertaken in 1968. Impervious cores with pervious shells were added to the downstream faces of both dams and a new spillway and outlet works were constructed at the north dam. The construction plans were reviewed, but design calculations were not studied.
- i. Normal Operating Procedures. No operating records are available. The outlet works normally remain closed.

#### 1.3 PERTINENT DATA

- a. <u>Drainage Area.</u> Halls Pond is located in northeast Connecticut and the watershed is rural and rolling in nature with only a few scattered homes. There are no significant storage areas to dampen the flows from the 1.3 square mile area.
- b. Discharge at Dam Site. There is no history of discharge data available for this dam. The following discharge data have been calculated with the calculations included in Appendix D.
  - 1. Outlet Works
    24" Concrete pipe, Invert
    Elev. 504.0
    Top of dam elevation 518.0 40 cfs
    Test flood elevation 516.3 40 cfs
  - 2. Maximum known flood Unknown

	з.	Ungated spillway capacity Top of dam elevation 518.0	430 cfs
	4.	Ungated spillway capacity Test flood elevation 516.3	200 cfs
	5.	Gated spillway capacity Normal pool elevation	N/A
	6.	Gated spillway capacity Test flood elevation 516.3	N/A
	7.	Total spillway capacity Test flood elevation 516.3	200 cfs
	8.	Total project discharge Top of dam elevation 518.0	470 cfs
	9.	Total project discharge Test flood elevation 516.3	240 cfs
c.	Ele	evation. (feet above NGVD)	
		NORTH DAM	
	1.	Streambed at toe of dam	501.0
	2.	Bottom of cutoff	None
	з.	Maximum tailwater	Unknown
	4.	Normal pool	514.0
	5.	Full flood control pool	N/A
	6.	Spillway crest	514.0
	7.	Design surcharge	517.0
	8.	Top of dam	518.0
	9.	Test flood surcharge	516.3

# SOUTH DAM

	1.	Streambed at toe of dam	503.5
	2.	Bottom of cutoff	None
	з.	Maximum tailwater	N/A
	4.	Normal pool	514.0
	5.	Full flood control pool	N/A
	6.	Spillway crest	None
	7.	Design surcharge	517.0
	8.	Top of dam	517.5
	9.	Test flood surcharge	516.3
d.	Res	servoir. (Length in feet)	
	1.	Normal pool	3,500
	2.	Flood control pool	N/A
	з.	Spillway crest pool	3,500
	4.	Top of dam	3,500
	5.	Test flood pool	3,500
e.	Sto	rage. (Acre-Feet)	
	1.	Normal pool	550
	2.	Flood control pool	N/A
	з.	Spillway crest pool	550
	4.	Top of dam	890
	5.	Test flood pool	750

## f. Reservoir Surface. (Acres)

Normal pool
 Flood control pool
 Spillway crest

4. Test flood pool 84

5. Top of dam 85

#### g. Dam.

#### NORTH DAM

1. Type
Original dam
Earth fill with masonry faces

Added

Downstream importances

dded Downstream impervious core and pervious shell

2. Length 250'

3. Height 23.5'

4. Top width

5. Side slope 2H:1V

6. Zoning Impervious core added but

does not meet requirements of Bureau of Reclamation for width to be considered a

zoned structure

7. Impervious core Top width varies 5' to 8'

with slopes 1H:2V

8. Cutoff Unknown

9. Grout curtains Unknown

#### SOUTH DAM

1. Type Original Earth dike Added Downstream impervious core and pervious shell 2. Length 2501 3. Height 141 Top width 4. 14' 5. Side slopes 2H:1V 6. Zoning Impervious core added but does not meet requirements of Bureau of Reclamation for width to be considered a zoned structure 7. Impervious core Top width 4', U.S. slope negative 1H:2V and D.S. slope 1H:1V 8. Cutoff Unknown 9. Grout curtains Unknown h. Diversion of Regulating Tunnel. N/A Spillway. 1. Type Twin 9'x3.3' concrete box culvert 2. Length of weir 181 3. Crest elevation 514.0 4. Gates None 5. U/S Channel Natural Bed 6. D/S Channel Concrete chute

i.

# j. Regulating Outlets.

1. Invert

504.0

2. Size

24"

3. Description

Concrete pipe

4. Control mechanism

Metal slide gate

5. Other

Contained in brick gate house

# SECTION 2 - ENGINEERING DATA

#### 2.1 DESIGN

Design data for the original dam is not available. Design data for the 1968 construction was not reviewed.

## 2.2 CONSTRUCTION

No record of the original construction is available

#### 2.3 OPERATION

No operating records are available.

### 2.4 EVALUATION

- a. <u>Availability</u>. Construction plans for the 1968 construction were supplied. Original design data and construction plans are not available.
- b. Adequacy. A definitive review was not made.
- c. Validity. The validity of available data should be verified if a definitive review is to be performed.

#### SECTION 3 - VISUAL INSPECTION

#### 3.1 FINDINGS

- a. General. Based on visual inspection, the two Halls Pond Dams appear to be in fair condition.
- b. Dams.

#### NORTH DAM

- 1. Upstream Face The dumped rock fill is missing in some areas. There is minor brush growth, most of which has been trimmed as shown in Photos C1-1 and C1-6. There has been some erosion just south of the spillway, caused by storm runoff from the roadway.
- 2. Crest The crest consists of Kennerson Reservoir Road which is an oiled gravel Town road. The road is in good condition, but the wire rope guide rail on the west side has been partially removed at the south end as shown in Photo C1-1.
- 3. Downstream Face The downstream face is grass covered with some brush growth as shown in Photos C1-2 and C1-3.

  No seepage was observed.

#### SOUTH DAM

Upstream Face - The upstream face has dumped rock fill which
is missing in some areas as shown in Photos C2-3 and C2-4.
 There is minor areas from wave action.

- 2. Crest The crest is a gravel road in good condition as shown in Photo C2-2.
- 3. Downstream Face The downstream face is grass covered with some brush growth as shown in Photo C2-5. There is some seepage at the west end as shown in Photo C2-6.

  The seepage cannot be quantified without further investigation.

#### c. Appurtenant Structures.

- 1. Spillway Twin 9'x3.3' cast-in-place concrete box culverts constructed in 1968 form the spillway with a concrete channel on a 2H:1V slope for an outlet channel. Photos C1-4 and C1-5 show the spillway and channel. The spillway is in good condition except for a crack at the wingwall at the northwest corner as shown in Photo C1-4. This crack should be investigated further.
- 2. Outlet Works The outlet works consist of a 24 inch concrete pipe starting at the base of the upstream slope and running to a gate house just west of the road. A metal slide gate controls the flow and a 24 inch concrete outlet pipe discharges at the toe of slope at a concrete endwall. Photos C1-6, C1-7, C1-8, C1-9 and C1-10 show the outlet works are in good condition except that the gate house door hardware is badly rusted and the lock is inoperable. Since there is no lock on the control wheel, the operation of the outlet works

is susceptable to vandalism and unauthorized drawdown of the reservoir.

#### d. Reservoir Area.

No detrimental features in the reservoir area were observed during the visual inspection.

#### e. Downstream Channel.

At the north dam, the downstream channel is a natural stream called Slovik Brook as shown in Photo C1-11. At the south dam, an unnamed stream forms in a swampy area at the base of the dam as shown in Photo C2-7.

#### 3.2 EVALUATION

Based on the visual inspection, the overall condition of Halls Pond

Dams is fair with areas that require attention as outlined in Section 7.

#### SECTION 4 - OPERATIONAL AND MAINTENANCE PROCEDURES

#### 4.1 OPERATIONAL PROCEDURES

- a. General. This is a recreational pond that remains full during normal conditions. There is no other use of the water.
- b. Description of Any Warning System in Effect. There is no formal downstream warning system in case of emergency at the dam.

#### 4.2 MAINTENANCE PROCEDURES

- a. General. This dam is checked for maintenance requirements
  two times per year by District maintenance personnel and any
  required work is done at that time. Maintenance appears to be
  limited mainly to removal and trimming of vegetation.
- b. Operating Facilities. There does not appear to be any particular maintenance performed on the operating facilities.

#### 4.3 EVALUATION

The existing maintenance schedule should be continued and expanded to include the outlet facilities and rock dam faces.

5.1 GENERAL The north dam at Halls Pond is 250 feet long with a maximum height of 23.5 feet. There is a spillway consisting of twin 9'x3.3' box culverts and a 24" concrete pipe outlet.

The 1.3 square mile watershed is rolling and mainly wooded as shown in the overview photo. There are no significant storage areas in the watershed.

### 5.2 DESIGN DATA

When the 1968 construction was under design, the engineer determined that the time of concentration for Halls Pond is 85 minutes and the runoff coefficient is 0.34.

#### 5.3 EXPERIENCE DATA

No historical data for recorded discharges or water surface elevations is available for this dam or the watershed.

inspection of dams by the Corps of Engineers were used for the selection of the "Test Flood". Halls Pond is classified as small in size with a low hazard potential. Guidelines for these classifications recommend an event equal in magnitude to a storm of 50 year to 100 year return frequency. A 100 year storm was chosen for the test flood. The rational method was used with data developed when the 1968 reconstruction was designed.

The test flood was calculated to be 560 cfs with a peak outflow of 240 cfs. This outflow results in a water surface elevation of 516.3 which is 1.7 feet below top of dam. The capacity of the spillway at top of dam elevation is 430 cfs.

5.5 DAM FAILURE ANALYSIS At the north dam, applying the calculated dam failure discharge of 14,200 cfs when the water surface elevation is 518 (top of dam) will produce an approximate water surface elevation of 505.6 just downstream of the dam. Depths of flow would range from 11.1 feet just below the dam to 16.2 feet 2,500 feet downstream of the dam to 8.6 feet where Slovik Brook joins the Natchaug River 3,700 feet downstream. The only damage that would be done is to the roadway on the crest of dam. No buildings would be affected.

At the south dam, applying the calculated dam failure discharge of 9,200 cfs with the pond at top dam elevation will produce an approximate water surface elevation of 514.7 just below the dam. Depths of flow would range from 11.2 feet just below the dam to 4.0 feet 2,500 feet downstream of the dam. No houses, other structures or roads would be damaged.

Halls Pond Dams are classified as having a low hazard because no structures would be damaged. Computations of water surface elevations and a map showing the limits of the impact area are included in Appendix D.

#### SECTION 6 - STRUCTURAL STABILITY

- 6.1 <u>VISUAL OBSERVATION</u> The field inspection did not reveal any stability problems.
- 6.2 <u>DESIGN AND CONSTRUCTION DATA</u> There is no design or construction information available for the original dam construction to permit a formal evaluation of the stability of the dam. Thus, the evaluation of stability is based solely on the visual inspection and the construction plans for the 1968 work.
- 6.3 POST CONSTRUCTION CHANGES There are no post construction changes apparent except for the 1968 construction.
- 6.4 <u>SEISMIC STABILITY</u> Halls Pond Dams are located in Seismic Zone

  1 and in accordance with Corps of Engineers guidelines do not warrant further seismic analysis at this time.

# SECTION 7 - ASSESSMENT, RECOMMENDATIONS AND REMEDIAL MEASURES

# 7.1 DAM ASSESSMENT

- a. <u>Condition</u>. Based on the visual inspection, Halls Pond Dams appears to be in fair condition.
- b. Adequacy of Information. The lack of in-depth engineering data did not allow for a definitive review. Therefore, the adequacy of these dams could not be assessed from the standpoint of reviewing design and construction data, but is based primarily on the visual inspection, plans for 1968 construction, past operational performance of the structure, and sound engineering judgement.
- c. <u>Urgency</u>. The recommendations presented in Section 7.2 should be carried out within one year of receipt of this report by the Owner and the remedial measures presented in Section 7.3 within two years.

# 7.2 RECOMMENDATIONS

It is recommended that the Owner employ a qualified registered engineer to:

- a. Investigate areas of seepage in the downstream face of the south dam to determine if repairs are warranted.
- b. Investigate the crack in the box culvert spillway at the northwest corner to determine if repairs are warranted.

#### 7.3 REMEDIAL MEASURES

- a. Operation and Maintenance Procedures.
  - 1. Repair guide rail at south end of north dam.
  - 2. Construct paved ditch to carry road water at spillway.
  - 3. Paint all steel in gate house and repair lock on door.
  - 4. Repair riprap at both dams.
  - 5. Check operation of gate on a regular basis.

#### 7.4 ALTERNATIVES

There are no practical alternatives to the recommendations and remedial measures in Sections 7.2 and 7.3.

# APPENDIX A

INSPECTION CHECK LIST

# VISUAL INSPECTION CHECK LIST PARTY ORGANIZATION

PROJECT Halls Pond	DATE2/27/81
North Dam	
	TIME 11:00 a.m.
	WEATHER Clear - 45°
•	W.S.Elev. 514.0 U.S.495.0 DN.S.
PARTY:	
1. G. Mirtl, Hydrology & Hydrau	ulics 6.
2. E. Lang, Structural & Mechan	nical 7.
3. S. Marniki, Soils & Geology	8
4	9
5.	10
PROJECT FEATURE	INSPECTED BY REMARKS
1	•
2.	
3	
5.	
8	
9.	
10.	

PROJECT Halls Pond - North .	DATE 2/27/81
PROJECT FEATURE	NAME
DISCIPLINE	NAME
AREA EVALUATED	CONDITION
DIKE EMBANKMENT	
Crest Elevation	518.0
•	
Current Pool Elevation	514.0
Maximum Impoundment to Date	Unknown
Surface Cracks	None
Pavement Condition	Good
	·
Movement or Settlement of Crest	None
Lateral Movement	None
•	
Vertical Alignment	Good
Horizontal Alignment	Good
	-
Condition at Abutment and at	
Concrete Structures	Some erosion S.W. side of inlet
	wingwall
Indications of Movement of	
Structural Items on Slopes	None
A-2	·

PROJECT Halls Pond - North	DATE2/27/81
PROJECT FEATURE	NAME
DISCIPLINE	NAME
·	·
AREA EVALUATED	CONDITION
DIKE EMBANKMENT (cont)	
Trespassing on Slopes	Fisherman use U.S. slope
Sloughing or Erosion of Slopes or Abutments	Minor from wave action and road road runoff
Rock Slope Protection — Riprap Failures	Some stone missing
Unusual Movement or Cracking at or near Toes	None
Unusual Embankment or Downstream Seepage	None
Piping or Boils	None
Foundation Drainage Features	None
Toe Drains	None
Instrumentation System	None
Vegetation	Some small trees D.S. slope

PROJECT Halls Pond - North	DATE2/27/81
PROJECT FEATURE	NAME
DISCIPLINE	NAME
•	
AREA EVALUATED	CONDITION
OUTLET WORKS - INTAKE CHANNEL AND INTAKE STRUCTURE	
a. Approach Channel	Pipe under water
Slope Conditions	
Bottom Conditions	
Rock Slides or Falls	
Log Boom	
Debris	
Condition of Concrete Lining	
Drains or Weep Holes	
b. Intake Structure	
Condition of Concrete	Good
	· .
Stop Logs and Slots	Good
A-4	

PROJECT Halls Pond - North	DATE _	2/27/81
PROJECT FEATURE	NAME_	
DISCIPLINE	NAME_	·
AREA EVALUATED		CONDITION
OUTLET WORKS - TRANSITION AND CONDUIT	Pipe	
General Condition of Concrete	Good	
Rust or Staining on Concrete	None	
Spalling	None	
Erosion or Cavitation	None	
Cracking	None	
Alignment of Monoliths	N/A	
Alignment of Joints	N/A	
Numbering of Monoliths	N/A	
		••
A-5		

PROJECT Halls Pond - North	DATE2/27/81
PROJECT FEATURE	NAME
DISCIPLINE	NAME
	•
AREA EVALUATED	CONDITION
OUTLET WORKS - CONTROL TOWER	·
a. Concrete and Structural	
General Condition	Good
Condition of Joints	Good
Spalling	None
Visible Reinforcing	None
Rusting or Staining of Concrete	None
Any Seepage or Efflorescence	None
Joint Alignment	Good
Unusual Seepage or Leaks in Gate Chamber	None observed
Cracks	None observed
Rusting or Corrosion of Steel	Door hardware rusting
	••

PROJECT Hails Pond - North	DATE2/27/81
PROJECT FEATURE	NAME
DISCIPLINE	NAME
,	
AREA EVALUATED	CONDITION
OUTLET WORKS - CONTROL TOWER (cont)	
b. Mechanical and Electrical	No electrical
Air Vents	Good
Float Wells	N/A
Crane Hoist	N/A
Elevator	N/A
Hydraulic System	N/A
. Service Gates .	Some rusting of control wheel not secured from unauthorized use.
Emergency Gates	N/A
Lightning Protection System	N/A
Emergency Power System	N/A
Wiring and Lighting System	N/A
,	•

PROJECT Halls Pond - North	DATE _	2/27/81
PROJECT FEATURE	NAME _	
DISCIPLINE	NAME_	•
		•
AREA EVALUATED		CONDITION
OUTLET WORKS - OUTLET STRUCTURE AND OUTLET CHANNEL	Pipe	
General Condition of Concrete	Good	
Rust or Staining	None	,
Spalling	None	
Erosion or Cavitation	None	
, Visible Reinforcing	None	
Any Seepage or Efflorescence	None	
Condition at Joints	Good	
Drain Holes	None	•
Channel	Good	
Loose Rock or Trees Overhanging Channel	None	,
Condition of Discharge Channel	Good	
<b>A</b> 0		

PROJECT Halls Pond - North	DATE _	2/27/81
PROJECT FEATURE	_ NAME _	
DISCIPLINE	NAME	
AREA EVALUATED		CONDITION
OUTLET WORKS - SPILLWAY WEIR,  APPROACH AND DISCHARGE  CHANNELS		
a. Approach Channel	•	•
General Condition	Good	
Loose Rock Overhanging Channel	N/A	
Trees Overhanging Channel	None	·
Floor of Approach Channel	Good	
b. Weir and Training Walls		
. General Condition of Concrete	Good	
Rust of Staining	None	
Spalling	None	
Any Visible Reinforcing	None	
Any Seepage or Efflorescence	None	· .
	ļ	

PROJECT Halls Pond - North	DATE 2/27/81
PROJECT FEATURE	NAME
DISCIPLINE	NAME
AREA EVALUATED	CONDITION
OUTLET WORKS - SPILLWAY WEIR,  APPROACH AND DISCHARGE  CHANNELS	
b. Weir and Training Walls	
Drain Holes	None ·
c. Discharge Channel	
General Condition	Good .
-	
Loose Rock Overhanging Channel	Noné
Trees Overhanging Channel	None
Floor of Channel	Good
Other Obstructions	Some debris at end of channel.
A-10	

PROJECT	DATE <u>2/27/81</u>
PROJECT Halls Pond - North	
PROJECT FEATURE	NAME
DISCIPLINE	NAME
AREA EVALUATED	CONDITION
OUTLET WORKS - SERVICE BRIDGE	N/A ·
a. Super Structure	
Bearings	
Anchor Bolts	
Bridge Seat	
Longitudinal Members	
Under Side of Deck	
Secondary Bracing	
Deck	
Drainage System	
Railings	
Expansion Joints	
Paint A-11	

	•
PROJECT Halls Pond - North	DATE 2/27/81
PROJECT FEATURE	NAME
DISCIPLINE	NAME
AREA EVALUATED	CONDITION
OUTLET WORKS - SERVICE BRIDGE (cont)	N/A
b. Abutment & Piers	
• · · · · · · · · · · · · · · · · · · ·	
General Condition of Concrete	
Alignment of Abutment	·
Approach to Bridge	
Condition of Seat & Backwall	
	·
	• •
	•
	•
•	·
, •	
	••
·	

A-12

# VISUAL INSPECTION CHECK LIST PARTY ORGANIZATION

PROJECT Hatts Pond - South Dan	DATE 2/27/81
	TIME 10:00 a.m.
	WEATHER Clear - windy - 40°
· ·	W.S.Elev. 514.0 U.S. None DN.S.
PARTY:	
	lics6.
	nical7.
	8
4	
5	
	INSPECTED BY REMARKS
1	•
2.	· ·
4.	
5.	
6.	
7.	
8.	
9.	
10.	

PROJECT Halls Pond - South	DATE 2/27/81
PROJECT FEATURE	NAME
DISCIPLINE	NAME
AREA EVALUATED	CONDITION
DIKE EMBANKMENT	
Crest Elevation	517.5
	•
Current Pool Elevation	514.0
Maximum Impoundment to Date	Unknown
Surface Cracks	None
Pavement Condition	Good
Movement or Settlement of Crest	None
Lateral Movement	None
Vertical Alignment	Good
Horizontal Alignment	Good
Condition at Abutment and at Concrete Structures	N/A
Indications of Movement of Structural Items on Slopes	N/A
A 44	

PROJECT Halls Pond - South	DATE2/27/81
PROJECT FEATURE	NAME
DISCIPLINE	NAME
AREA EVALUATED	CONDITION
DIKE EMBANKMENT (cont)	
Trespassing on Slopes	Fisherman on U.S. slope
Sloughing or Erosion of Slopes or Abutments	Some erosion U.S. from wave action
Rock Slope Protection - Riprap Failures	Some riprap missing above normal water level U.S.
Unusual Movement or Cracking at or near Toes	None
Unusual Embankment or Downstream Seepage	Some seepage west end at base of slope
Piping or Boils	None
Foundation Drainage Features	Toe Drain
Toe Drains	Appear to be operating
Instrumentation System	None
Vegetation	Small brush both sides
	••

PROJECT Halls Pond - South	DATE 2/27/81
PROJECT FEATURE	NAME
DISCIPLINE	NAME
	•
AREA EVALUATED	CONDITION
OUTLET WORKS - INTAKE CHANNEL AND INTAKE STRUCTURE	N/A
a. Approach Channel	
Slope Conditions	
Bottom Conditions	
Rock Slides or Falls	
Log Boom	
Debris	
Condition of Concrete Lining	
. Drains or Weep Holes	
b. Intake Structure	
Condition of Concrete	
Stop Logs and Slots	

PROJECT Halls Pond - South	DATE	2/27/81
PROJECT FEATURE	_ NAME	
DISCIPLINE	NAME_	•
AREA EVALUATED	<u> </u>	CONDITION
OUTLET WORKS - TRANSITION AND CONDUIT	N/A	
General Condition of Concrete		
Rust or Staining on Concrete		
Spalling		
Erosion or Cavitation		
Cracking		
Alignment of Monoliths		
Alignment of Joints		
Numbering of Monoliths		
	•	
A-17		

PROJECT Halls Pond - South	DATE _	2/27/81
PROJECT FEATURE	NAME_	
DISCIPLINE	NAME	
		•
	• • • •	CONDITION
AREA EVALUATED		CONDITION
OUTLET WORKS - CONTROL TOWER	N/A	
a. Concrete and Structural		,
General Condition	•	
Condition of Joints		
Spalling		
Visible Reinforcing		
Rusting or Staining of Concrete		
Any Seepage or Efflorescence		
Joint Alignment		
Unusual Seepage or Leaks in Gate Chamber		
Cracks		
Rusting or Corrosion of Steel		

PROJECT Halls Pond - South	_ DATE _	2/27/81
PROJECT FEATURE	_ NAME	
DISCIPLINE	NAME	· .
		•
AREA EVALUATED		CONDITION
OUTLET WORKS - CONTROL TOWER (cont)	N/A	
b. Mechanical and Electrical	•	
Air Vents		
Float Wells		
Crane Hoist		
Elevator		
Hydraulic System		·
Service Gates		
Emergency Gates		
Lightning Protection System		
Emergency Power System		
Wiring and Lighting System	·	
A-19		

PROJECT Halls Pond - South	DATE	2/27/81	
PROJECT FEATURE	_ NAME		
DISCIPLINE	NAME		·
		•	
AREA EVALUATED		CONDITION	. <u>.                                   </u>
OUTLET WORKS - OUTLET STRUCTURE AND OUTLET CHANNEL	N/A		
General Condition of Concrete	•		
Rust or Staining			
Spalling			
Erosion or Cavitation			
, Visible Reinforcing			
Any Seepage or Efflorescence			
Condition at Joints			
Drain Holes		•	
Channel			
Loose Rock or Trees Overhanging Channel	٠.		
Condition of Discharge Channel		• •	
A-20			

PROJECT Halls Pond - South	_ DATE _	2/27/81
PROJECT FEATURE	_ NAME_	
DISCIPLINE	_ NAME_	
AREA EVALUATED		CONDITION
OUTLET WORKS - SPILLWAY WEIR,  APPROACH AND DISCHARGE  CHANNELS	N/A	
a. Approach Channel	•	•
General Condition		
Loose Rock Overhanging Channel		
Trees Overhanging Channel		
Floor of Approach Channel		
b. Weir and Training Walls		
. General Condition of Concrete		
Rust of Staining		
Spalling	.,	
Any Visible Reinforcing		·
Any Seepage or Efflorescence		•
A-21	. 7,	

PROJECT Halls Pond - South	DATE 2/27/81
PROJECT FEATURE	NAME
DISCIPLINE	NAME
AREA EVALUATED	CONDITION
OUTLET WORKS - SPILLWAY WEIR,  APPROACH AND DISCHARGE  CHANNELS	N/A
b. Weir and Training Walls	
Drain Holes	•
c. Discharge Channel	
General Condition	•
Loose Rock Overhanging Channel	•
Trees Overhanging Channel	
Floor of Channel	
Other Obstructions	

PROJECT Halls Pond - South	DATE	2/27/81
PROJECT FEATURE		,
DISCIPLINE	<del> </del>	
DISON CHAL		
AREA EVALUATED		CONDITION
OUTLET WORKS - SERVICE BRIDGE	N/A	
a. Super Structure		
Bearings		•
Anchor Bolts		•
Bridge Seat	·	
Longitudinal Members		
Under Side of Deck		
Secondary Bracing		
Deck		
Drainage System		
Railings		
Expansion Joints		
Paint		

PROJECT Halls Pond - South	DATE 2/27/81
PROJECT FEATURE	NAME
DISCIPLINE	NAME
AREA EVALUATED	CONDITION
OUTLET WORKS - SERVICE BRIDGE (cont)	N/A
b. Abutment & Piers	
General Condition of Concrete	
Alignment of Abutment	
Approach to Bridge	
Condition of Seat & Backwall	
	•
•	
	•

A-24

### APPENDIX B

ENGINEERING DATA

HALLS POND NORTH DAM

SECTION AT SPILLWAY

SCALE: 1"= 10"

# HALLS POND

# SECTION AT OUTLET WORKS

SCALE: 1"= 10"

HALLS POND SOUTH DAM

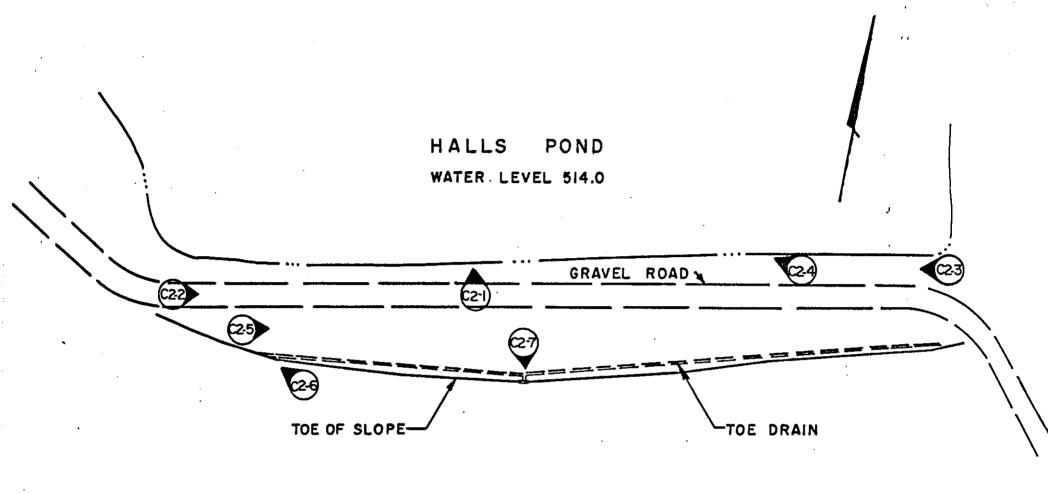
PLAN

SCALE: | "= 40"

		•	- 1 3 /s	<i>(</i>
No.		WATER RESOURCES UNIT SUPERVISION OF DAMS		50.6'
-	itoried	INVENTORY DATA	south dam: Lat: 41 <sup>0</sup> 50.2' Long: 72 <sup>0</sup> 6.5'	
			<b>3</b>	,
Date		d HALLS POND (No	orth Dam - {2} dams}	
	,			
•	Town Eastford			
	·	Hampton		
٠		<del></del>		
	Name of Stream			
	Owner State of		<del></del>	
	Address VEP	· · · · · · · · · · · · · · · · · · ·		
			South Chaplin	
ilt 1	968			
	Pond Used For		Drainage Area	
	Dimensions of Pond	d: Width	Length Area8	
	Total Length of Da	um <u>8=450</u> 1	Length of Spillway 19'	
	Location of Spillw	vay		
	Height of Pond Abo	ove Stream Bed <u>16' n</u>	rorth none-south	<del></del>
	Height of Embankme	ent Above Spillway <u>5'</u>	north .	
-	Type of Spillway (	Construction <u>concrete</u>	e (north)	<del></del>
	Type of Dike Const	truction <u>earth (s)</u>	earth cover with riprap (n)	
	Downstream Condit	ions woods, pond, road	d south	<del></del>
•	•	woods, farm, road no		<u>.</u>
·	Summary of File Da	ata F&G asked to re	epair leak Feb. 63; modification	u
• :		sign March 62		
•			in good condition. The north o	lam i
			upstream face. Kennersen Road	
			. The concrete spillway is also	
	condition V	B Can Damaga? YES	Class	С

## APPENDIX C

**PHOTOGRAPHS** 



HALLS POND SOUTH DAM

PLAN

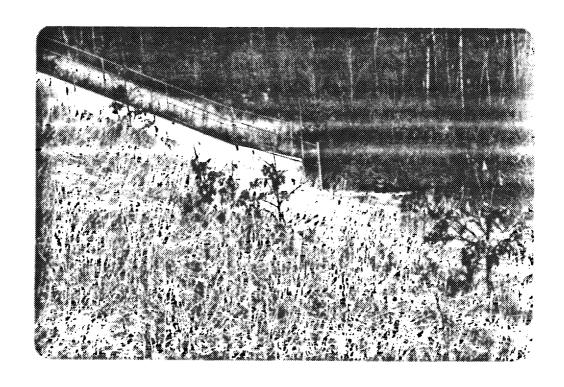
SCALE:1"= 40'



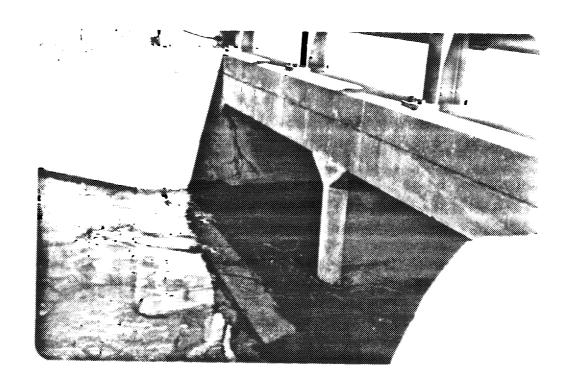
C1-1 UPSTREAM SLOPE



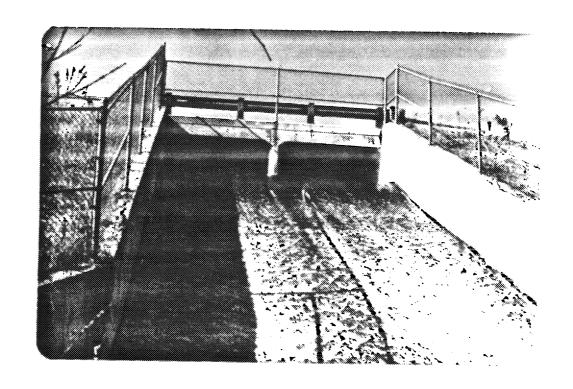
C1-2 DOWNSTREAM SLOPE



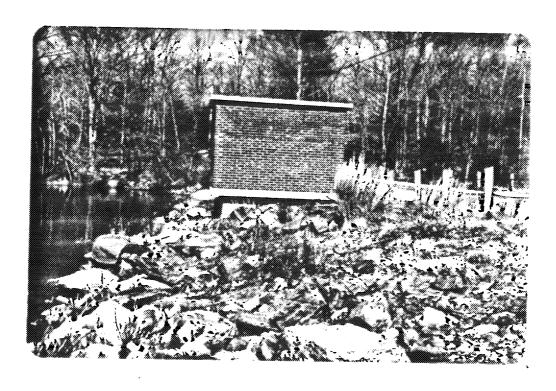
C1-3 DOWNSTREAM SLOPE AT SPILLWAY



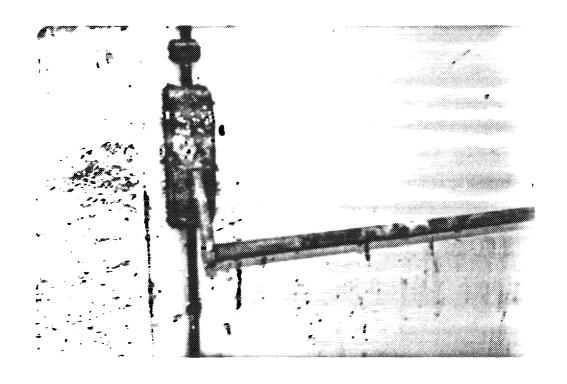
C1-4 UPSTREAM END OF SPILLWAY



C1-5 DOWNSTREAM END OF SPILLWAY



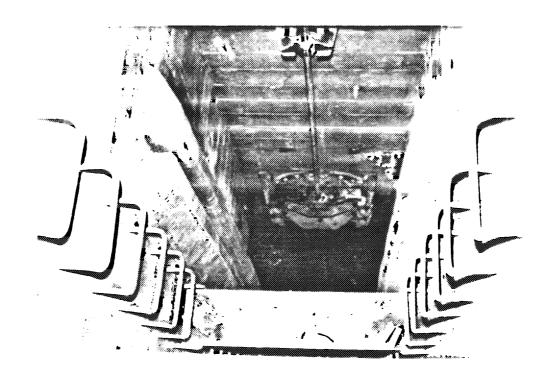
C1-6 GATEHOUSE



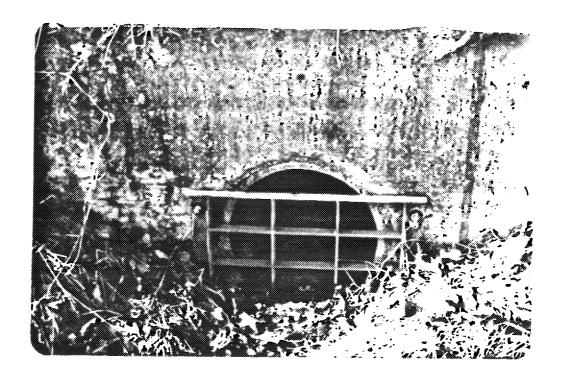
C1-7 GATEHOUSE DOOR LATCH



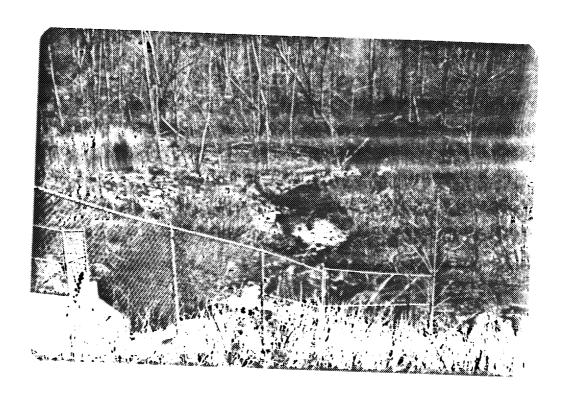
C1-8 GATE CONTROL WHEEL



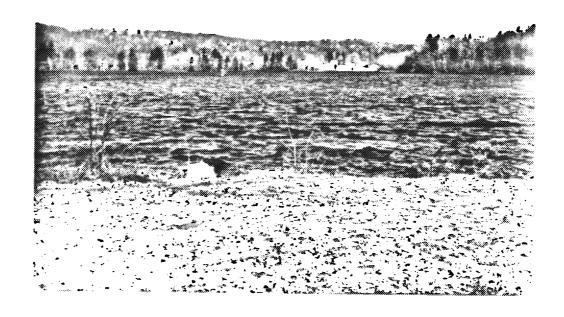
C1-9 GATE PIT



C1-10 OUTLET CONDUIT



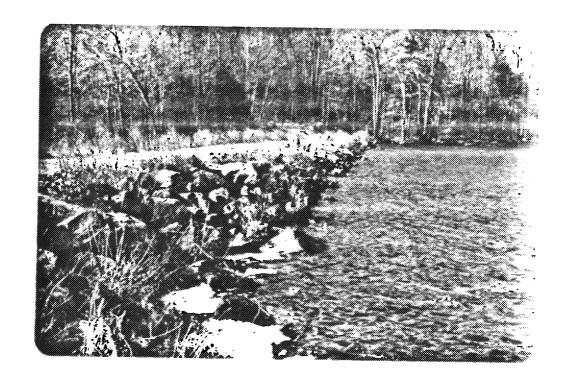
C1-11 DOWNSTREAM CHANNEL



C2-1 POND LOOKING NORTH



C2-2 DIKE CREST



C2-3 UPSTREAM FACE



C2-4 MISSING RIPRAP ON UPSTREAM FACE



C2-5 DOWNSTREAM FACE



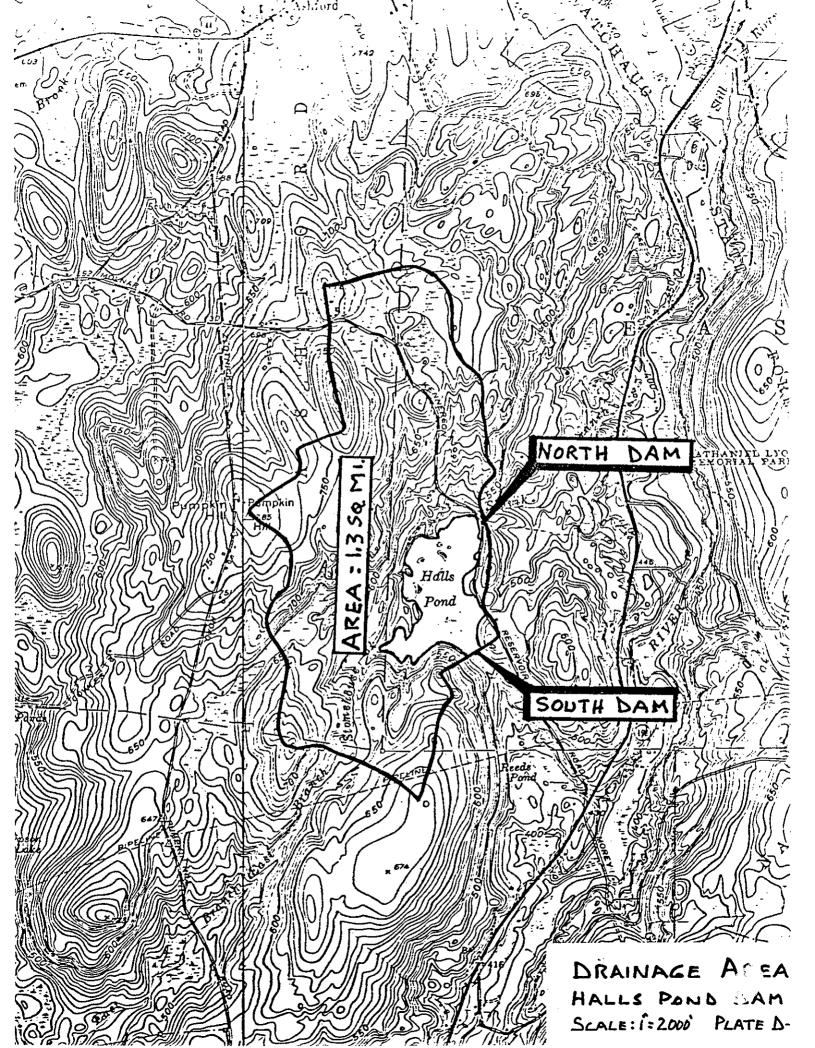
C2-6 SEEPAGE ON DOWNSTREAM FACE

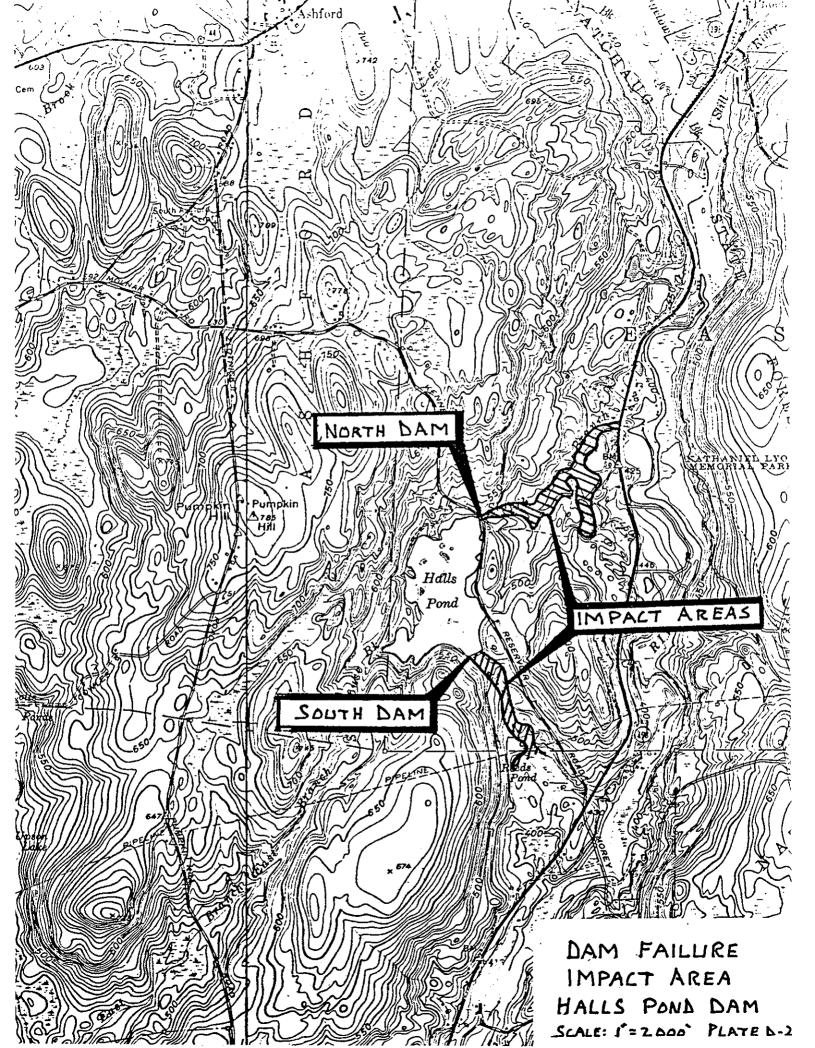


C2-7 DOWNSTREAM CHANNEL

## APPENDIX D

HYDROLOGIC AND HYDRAULIC COMPUTATIONS







PREPARED C-ZW BY

DATE

CHECKED

DATE

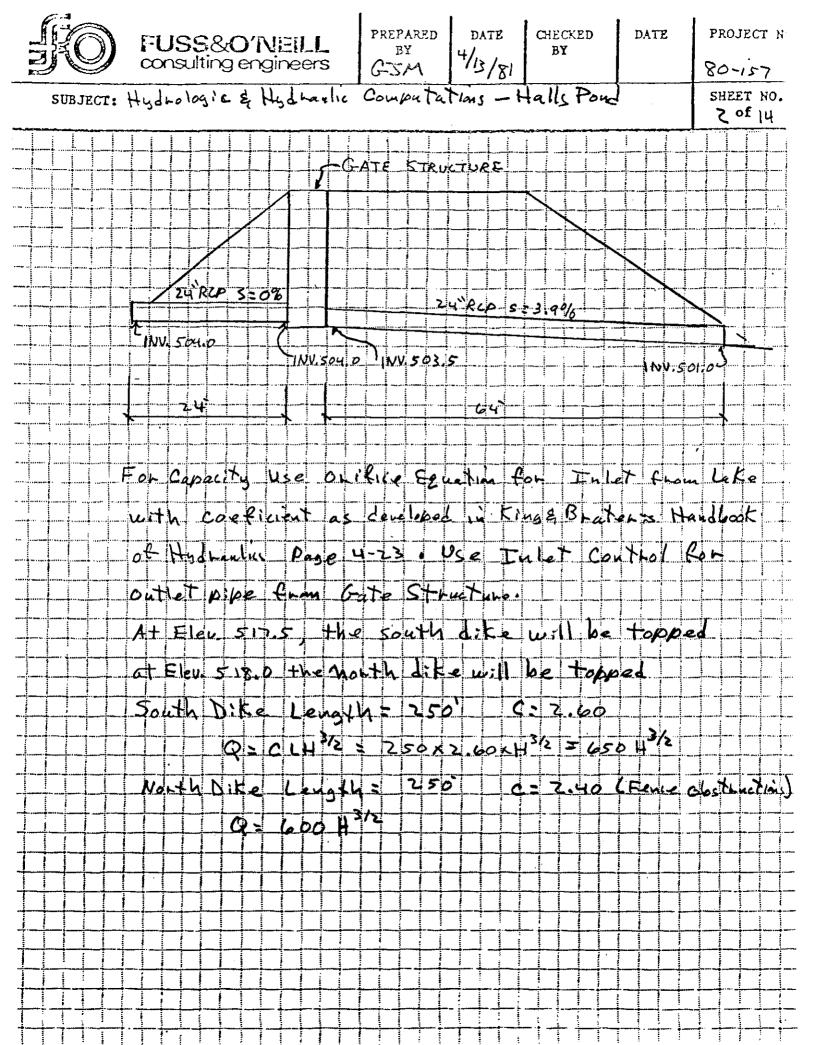
PROJECT NO 80-157

SUBJECT: Hydrologic & Hydraulic Computations - Halls Pand

SHEET NO.

Watershad Slope - Rolling Storage Volume: Surface Area at Spillway Elep. = 82.3 Ac Ave. Depth = 6.7 Ft. Volume = 82.3 x 6.7 = 550 A. FX Debth from Spillway to Top of Dam = 4.0 Volume= 85x4,5= 340 Ac. Ft. Total Storage = 890 Ac. Ft. Size Classification = Small Use 100 Yr. Engluency Storm For Tost Flood Following Information Developed For 1968 Reconstruction of Dani Drainage Aven: 820 Ac
Time of Concentration = 85Min
Runoff Coefficient = 0.34 From Conn. D.O. T. Drainage Manuel 100 Yr. Rainfall = 2.0 /hr Q100 = 820x 6.34 x 2.0 = 560 cfs. Effect of Surcharge Storage Ungated Spillway = Twin a Wile Box Culvert with
Height = 4.3 at Entrance Use Inlet Control For Capacity with Invent = Elev. 514. Gated Outlet = Z4 RCP Wit 15 Endwah

Invert = 504.0 at Intake Threnta 503. 5 at Outlet from Gate Structure





PREPARED BY G-3M

DATE 4/3/8/ CHECKED BY

DATE

PROJECT N

80-157

SUBJECT: Hydrologic & Hydraulic Computations - Halls Pond

Summary of Nischerge Floors  ELEU Linguish Gated South Dike North Dike To Structure Structure Overflow  Structure Structure Overflow  SINO 170 cls 40 0 0 0 22  \$17.0 280 40 0 0 32  \$18.5 500 50 650 70  \$18.5 500 50 650 70  \$18.0 560 50 190 600 246  Qpi = 560 cls  Suchange Height to Dass Qpi = 517.6 (3.6)  Volume of Sumhange = 570K = 854c x3.6 = 206.0 Ac. Ft  Drumage Area 1.3 Sp. M. = 830 Ac.  306 4830 x12 4.4 1.1 Runoff  100 Year Runoff = 5.2  Qpz = 560 (1 - 5.2) = 80 cls  Suchange Height to Dass Qpi = 517.9 (0.91)  Volume of Suchange = 570K2 = 85 to 9 = 76.5 Ac. Ft  76.5 1830 x12 1.1 Runoff  Area 570K & 570K2 = (306 + 76.5) = 25 191 Ac.  Sachange = 23° (Fleu S16.3)  Qpz = 243 Cls				س.ه	. <b>Q</b> .I	۸5		. ط	£	1	J	Ī	1		•						<del>-</del>					1			-	,	7
5100 170 cfs 40 0 0 0 32  517.0 280 40 0 0 33  518.0 430 40 730 6 70  518.5 500 50 650 210 14  519.0 560 50 1190 600 24  Qp = 560 cfs  Suchange Height to pass Qp = 517.6 (3.6)  Volume of Sumhange = STOR1 = 85Ac x3.6 = 306.0 Ac. Ft  Drainage Axa 1.3 Sp. M1 = 830 Ac  306 = 830 x12 = 4.4 in. Runoff  100 Year Runoff = 5.2  Qp = 560 (1 - 5.2) = 90 cfs  Surchange Height to pass Qo; 514.9 (0.9)  Volume of Suchange = STOR2 = 85 x0 9 = 76.5 Ac. Ft  76.5 1350 x12 = 1.1 Runoff  Ave. STOR, & STOR2 = (306 + 76.5) = 2 = 191 Ac.	L٤		♣	:		:	i			· · · · · ·	٦١	.Z.C.	h	٠.	8		ء ا	دد	2					<u>.</u>	┿-		<u> </u>	1			-
517.0 280 40 0 32  518.0 430 40 230 8 70  518.5 500 50 650 210 141  519.0 560 50 1190 600 240  Qp_= 560 cfs  Surchange Height to pass Qp_= 517.6 (3.6)  Volume of Sumhange = 5TDR_= 854c x3.6 = 306.0 Ac. Ft.  Drainage Area 1.3 5e. M1 = 830 Ac.  306 830 x12 4.4 in. Runoff  100 Yan. Runoff 5.2  Qp_= 560 (1 - 5.2) = 90 cfs  Surchange Height to pass Qo2 514.9 (0.9)  Volume of Surchange = 5TOR2 = 85 x 0.9 = 76.5 Ac. Ft  76.5 830 x17 = 1.1 Runoff  Are STOR & STOR2 = (306 + 76.5) = 2 = 1911 Ac. Ft	 	<u> </u>		L S	ng th	at uc	i d	•		S	at tr	ed uct	44	P	S	0 u	th	ţ	ik	e										<b>T</b> 0	, , , , , , , , , , , , , , , , , , ,
518.0 430 40 730 6 70  518.5 500 50 650 210  519.0 560 50 1190 600  240  Qp. = 560 cfs  Sucharge Height to pass Qp. = 517.6 (3.6)  Volume of Sucharge = 5706, = 854c x3.6 = 306.0 Ac. Fth  Drainage Area 1.3 Se. M. = 830 Ac.  306 4830 x12 4.4 in Runoff  100 Yan Runoff = 5.2  Qp. = 560 (1 - 5.2) = 90 cfs  Sucharge Height to pass Qp. = 514.9 (0.9)  Volume of Sucharge = 57082 = 85 x0.9 = 76.5 Ac. Fth  76.5	رما ا	0			1	70	сf			-	L	0				_	(	2			_			<del> </del>	٥	-				2	
518.5 500 50 650 210 140  519.0 500 50 1190 600 240  Qp = 560 cfs  Suchange Height to pass Qp = 517.6 (3.6')  Volume of Suchange = 570R = 854c x3.6 = 306.0 Ac. Ft  Drainage Area 1.3 Se. M. = 830 Ac  306 = 830 x12 = 4.4 in. Runoff  100 Yan Runoff = 5.2'  Surchange Height to pass Qp = 514.9 (0.9')  Volume of Suchange = 570R2 = 85 x0.9 = 76.5 Ac. Ft  This is a solution = 1.1 Runoff  Ave. STOR, \$ 570R2 = (306 + 76.5) = 2 = 191 Ac.	517.	0			Z	80	-		-			10						2							<u>ا</u> ٥_					3	2
519.0 500 50 1190 600 240  Qp = 560 cfs  Surchauge Height to pass Qp = 517.6 (3.6')  Volume of Surchauge = STOR = 854c x3.6 = 306.0 Ac. Ft  Drainage Area 1.3 Se. M! = 830 Ac  306 + 830 x12 4.4 in. Runoff  100 Yan Runoff = 5.2'  Qp = 560 (1 - 5.2) = 90 cfs  Surchauge Height to pass Qp = 514.9 (0.9')  Volume of Surchauge = STOR = 85 x 0.9 = 76.5 Ac. Ft  765 + 830 x12 1.1 Runoff  Ave. STOR & STOR = (306 + 76.5) = 191 Ac. I	 518	مر	_		4	30			ļ		J	40					۷.	30							6					7.	<u>.</u>
Qp = 560 cfs  Suchange Height to pass Qp = 517.6 (3.6)  Volume of Sunhange = STDR = 85Ac x3.6 = 206.0 Ac. Fth  Drainage Area 1.3 Se. Mi = 830 Ac  306 = 830 x12 = 47.4 in. Runoff  100 Year Runoff = 5.2  Qp = 560 (1 - 5.2) = 90 cfs  Sunchange Height to pass Qp = 514.9 (0.9)  Volume of Sunchange = STOR2 = 85 x0.9 = 76.5 Ac. Fth  76.5 = 830 x12 = 1.1 Runoff  Ave. STOR = STOR2 = (306 + 76.5) = 2 = 191 Ac. Fth	518	.5			5	DC.	ļ					50					65	٥.						2	10	<u>.</u>				14	
Suchange Height to pass Qp = 517.6 (3.6)  Volume of Suchange = STDR = 854c x3.6 = 206.0 Ac. Ft  Drainage Avea = 1.3 Se. M! = 830 Ac.  306 = 830 x 12 = 41.4 in. Runoff  100 Year Runoff = 5.7  Qp2 = 500 (1 - 414) = 90 cfs  Suchange Height to pass Qp2 = 514.9 (0.9)  Volume of Suchange = STOR2 = 85 r0 9=76.5 Ar. Ft  76.5 = 880 x17 = 1.1 Runoff  Ave. STOR = 5TOR2 = (306 + 76.5) = 2 = 191 Ac. Ft  Suchange = 2.3 (Fleu 516.3)	519	٥.			S	60	j					<b>5</b> 0	>				ع ا	10							60	Ö				24	2
Volume of Sumhange = STOR, = 854c x3.6 = 206.0 Ac. Fh  Drainage Area = 1.3 Sg. M! = 830 Ac  306 = 830 x12 = 4.4 in. Runoff  100 Year Runoff = 5.2  Qp2 = 560 (1 - 5.2) = 90 cfs  Sumhange Height to pass Qp2 = 514.9 (0.91)  Volume of Sumhange = STOR2 = 85 x0.9 = 76.5 Ac. Ft  Are, STOR & STOR2 = (306 + 76.5) = 2 = 191 Ac. Ft  Sumhange = 2.3 (Flew 516.3)	Qp	, =		ی ک	,0	ے	£5																	ļ							
Volume of Sumhaus ? = STOR, = 854c x3.6 = 206.0 Ac. Fh  Drainage Area = 1.3 Sg. M! = 830 Ac  306 = 830 x12 = 4.4 in. Runoff  100 Year Runoff = 5.2  Qp2 = 560 (1 - 5.2) = 90 cfs  Sumhauge Height to pass 902 = 514.9 (0.91)  Volume of Sumhauge = STOR2 = 85 x 0.9 = 76.5 Ac. Ft  765 = 830 x12 = 1.1 Runoff  Are, STOR & STOR2 = (306 + 76.5) = 2 = 191 Ac. Ft  Sumhauge = 2.3 (Flew 516.3)	S۷	ماد	ho	2 - 6	, <u>e</u>	H	e i	g١	4.	1	0	Ą	as	ے د	Q	<b>6</b> 21	<b>=</b>	۱ ک	٦.	6	<u> </u>	لر :ن	3.6	2	)						
Drainege Area 1.3 Sq. MI = 830 Ac  306 + 830 x12 = 4.4 in. Runoff  100 Ygar Runoff = 5.2  Cp2 = 560 (1 - 5.2) = 90 cfs  Surchange Height to pass Qp2 = 514.9 (0.9')  Volume of Surchange = STOR2 = 85 + 0.9 = 76.5 Ar. Ft  76.5 = 830 x12 = 1.1 Runoff  Ave STOR & STOR2 = (306 + 76.5) = 2 = 191 Ac. F	.il		.i	.j	.i	İ					i		i							j	5				1	ن.	A	ς. J	<b>-</b> }		
306 = 830 x 12 = 4.4 in. Runoff  100 Year Runoff = 5.2  Qp2 = 560 (1 - 4.4 ) = 90 cfs  Surchange Height to pass Qp2 = 514.9 (0.9)  Volume of Surchange = STOR2 = 85 x 0.9 = 76.5 Ar. Ft  76.5 = 830 x 12 = 1.1 Runoff  Ave. STOR & STOR2 = (306 + 76.5) = 2 = 191 Ac. Ft  Surchange = 2.3 (Elev 516.3)					<u>. I</u>	<u>.</u>										<u>i</u>		j.,		<u>l</u>		<u>.i</u>		<del>!</del>						<u> </u>	-
100 Year Runoff = 5.2  Qp = 560 (1 - 5.2) = 90 cfs  Sunhange Height to pass Qp; 514.9 (0.9)  Volume of Sunhange = STOR2 = 85 + 0.9 = 76.5 Ac. Ft  76.5 + 830 xm = 1.1 Runoff  Ave. STOR & STOR2 = (306 + 76.5) = 2 = 191 Ac. P			ļ.,							`		;	i	- !	į		į	:	,	1.	i				ee						
Qp2 = 560 (1 - 5,2) = 90 cfs  Suchange Height to pass Qp2 = 514.9 (0.9)  Volume of suchange = 570R2 = 85 + 0.9 = 76.5 A1. Ft  765 = 830 ND = 1.1 Runoff  Ave. STOR & STOR = (306 + 76.5) = 2 = 191 Ac. 1  Sundange = 2.3 (Elev 516.3)		<u>.</u>																			<u>. į</u>										
Suncharge Height to pass 90; \$ 514.9 (0.9')  Volume of Sulcharge = STOR2 = 85 x 0.9=76.5 AL. Ft  76.5 x 830 x17 = 1.1 Runeff  Ave. STOR & STOR2 = (306 + 76.5) = 2 = 191 Ac. 1  Sulcharge = 2.3' (Elev 516.3)	(	<b>2</b> 0			5	6	O	7		_	1.	!	. :	•	:		į												-		
Volume of Suchange = STOR2 = 85 + 0.9 = 76.5 AL. FT  76.5 = 830 x17 = 1.1 Runeff  Ave. STOR, & STOR2 = (306. + 76.5) = 2 = 191 Ac. 1  Suichange = 2.3 (Elev. 516.3)		Ī	1	1	1	1		Ī	į	- 1	_ [	1	1	•		į	- 1	1	- 1	51	Ч.	9	1	0	9	• `					
76.5; 830 x17 = 1.1 Runoff  Ave. STOR, 5.5TOR2 = (306 + 76.5) = 2.1   91 Ac.1  Suchause = 2.3 (Elev. 516.3)			j		1	, -		Í				}	1	. 1	ŧ	- 1	1		į	1	1	1	1			;		1	. [		
Ave. STOR, & STOR; = (306. + 76.5) = 191 Ac.1 Swithauge = 2.3' ( & lev. \$16.3)							<i>-</i> 1				-		1	i	Ī		Ŧ	ì	ĺ	J	•			- 1							~
Suchauge = 2.3' ( Elev 516.3)			<u> </u>							ļ			Ì		į					1										-	
				A				1	7	1	1	į	1	~	1	1	Ì	1	į	1	1	į		)	:2	2	_1	91	_ /	40.	ŀ
Qp3 > 243 Cfs						S	4	بل	۱.4	ب	2	<b></b>	2	١3		7	Ę	e	U.	5 1	6.	37								1	-
				Q	۲۹	>	2	u	3	C	£5		_	1	_	_ -				1	<u> </u>					_					_
											-	- 1	1	1		_	-	-	1	-	1										<u>,                                    </u>



PREPARED BY CSM DATE 3/28/81

CHECKED BY DATE

PROJECT NO

80-157

SUBJECT: Dam Failure Hydrograph - Halls Pond South

STATION SLOPE M ELEVATION AREA Q  140 10% 100 510 650 2.00  515 1960 8.160 8.160  520 3910 24 800  540 6.7% 100 500 620 3.800  540 2.6% 100 475 650 1450 1450 1450  1540 3.196 1100 440 2.76 1900  1540 2.6% 100 440 2.70 900  2040 2.6% 100 440 300 955  2040 2.6% 100 440 300 955  2040 2.6% 100 440 300 955  2040 2.6% 100 440 300 955  2040 2.6% 100 440 300 955  2040 2.6% 100 440 300 956  2040 2.6% 100 440 300 956  2040 2.6% 100 440 300 956  2040 2.6% 100 446 300 956  2050 1000 1000	
140 106 100 510 650 7,000 9,600 515 1400 9,600 520 3310 24,800 520 52320 33,600 505 2320 33,600 1000 1475 650 4400 1480 1450 14,000 1480 1450 14,000 1450 14,000 1450 14,000 1450 14,000 1450 14,000 1	
15to 2.6% .100 510 650 7.100 9,600 515 1460 9,600 520 3310 24,800 520 524,800 520 33,600 505 2320 33,600 1620 2.6% .100 1435 650 1450 1450 1450 1450 1450 14,000 1455 1870 11,000 1455 1870 11,000 1455 1870 11,000 1495 1870 11,000 1495 1870 11,000 1495 1870 11,000 1495 1870 11,000	
515 1960 91,600 520 3916 24,800 540 6,7% 100 500 620 3,800 505 2320 30,600 10+0 2,6% 100 475 650 4400 480 1450 14,100 15+0 3,1% 100 440 770 900 745 1800 14,000 2010 2,6% 100 440 300 950 445 1800 14,900 25+6 0,8% 260 426 240 500 12,600	
515 1960 91,600 520 3316 24,800 3,800 3,800 3,800 3,800 3,800 3,800 3,800 3,800 3,800 3,800 3,800 3,800 1,0	
520 3910 24,800  570 6,7% 100 500 620 3,800  10+0 2.6% 100 475 650 4400 1450 1450 14,100  15+0 3.1% 100 400 270 900 15+0 3.1% 100 400 700 13,000  20+0 2.6% 100 440 300 950 1445 1800 4900 25+6 0.8% 100 426 240 500 12,000	-
5+0 6,7% 100 500 620 3,800  10+0 2,6% 100 475 650 4,400 1480 1450 14,100 1480 1450 14,100 1480 1450 14,000 20+0 2,6% 100 440 300 950 1485 1880 14,900 125+0 0,8% 100 420 240 540 550 14,000	
10+0   2,6%   100   475   450   440   1450   14,100   465   1370   14,000   465   1370   14,000   465   1860   14,900   430   2260   10,600   430   2260   10,600   430   2260   10,600   430   2260   10,600   430   2260   10,600   430   2260   10,600	
10+0   2,6%   100   475   450   440   1450   14,100   465   1370   14,000   465   1370   14,000   465   1860   14,900   430   2260   10,600   430   2260   10,600   430   2260   10,600   430   2260   10,600   430   2260   10,600   430   2260   10,600	
10+0   2,6%   100   1475   1450   1410   1480   1450   1410   1480   1450   1410   1	
10+0 2,6% 100 475 650 440 14,100 14,100 14,100 14,100 14,100 15+0 14,100	
10+0 2,6% 100 475 650 4400 14,100 14,100 14,100 14,100 14,100 14,100 14,100 14,100 14,100 14,100 14,100 14,100 14,100 14,100 12,100 14,	
15+0 3.1% .100 440 2.70 900 15,000 445 1870 11,000 26% .000 445 1800 4490 25+0 0.8% .000 426 240 500 10,000	
15+0 3.1% .100 440 2.70 900 15,000 445 1870 11,000 26% .000 445 1800 4490 25+0 0.8% .000 426 240 500 10,000	
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2010 2 6%, 108 440 200 956 445 1800 14,900 25+6 0.8% 000 436 240 500 19600	
20+0 2.6% 10a 44e 300 950 11,900	
2010 2 6% 100 440 300 950 41,900 11,900 12,600 12,600 12,600	
25t6 0.8% 200 430 240 5teo 10,000	
25t6 0.8% 060 430 240 5teo 10,000	
25ts 0.8% 060 430 210 5teo 10,000	
2-5+6 0.8% 060 430 220 10,600 130 220 10,600	
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PREPARED

DATE

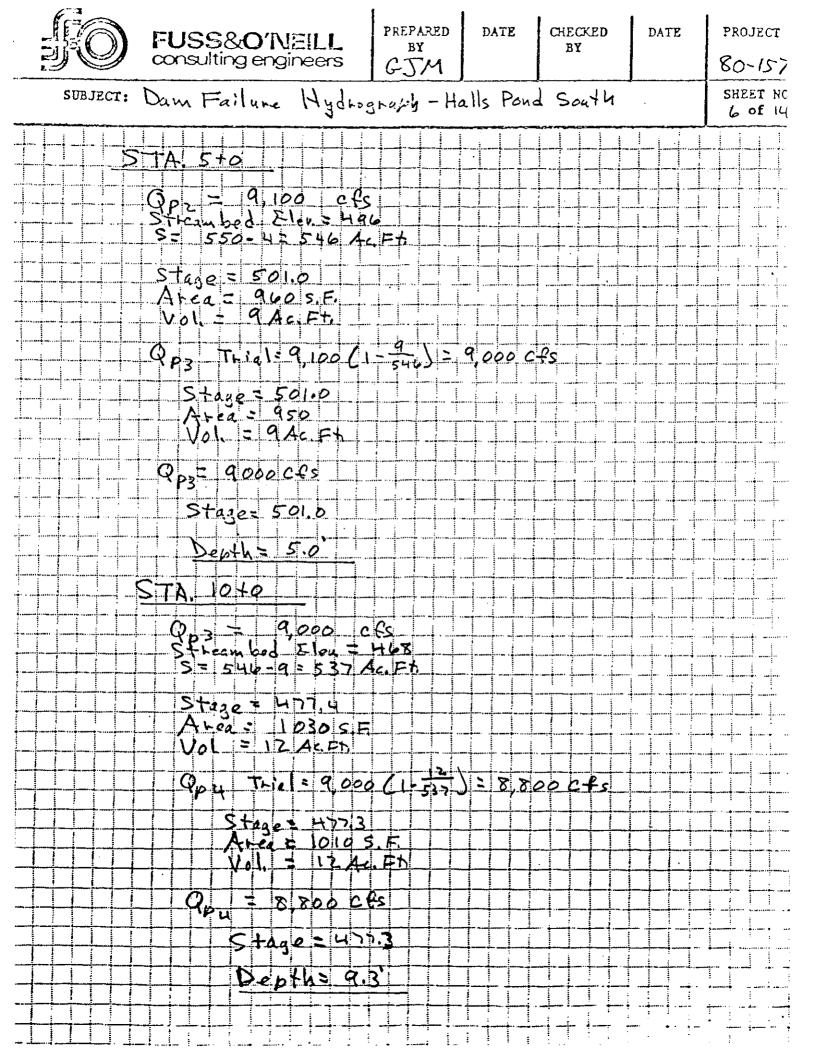
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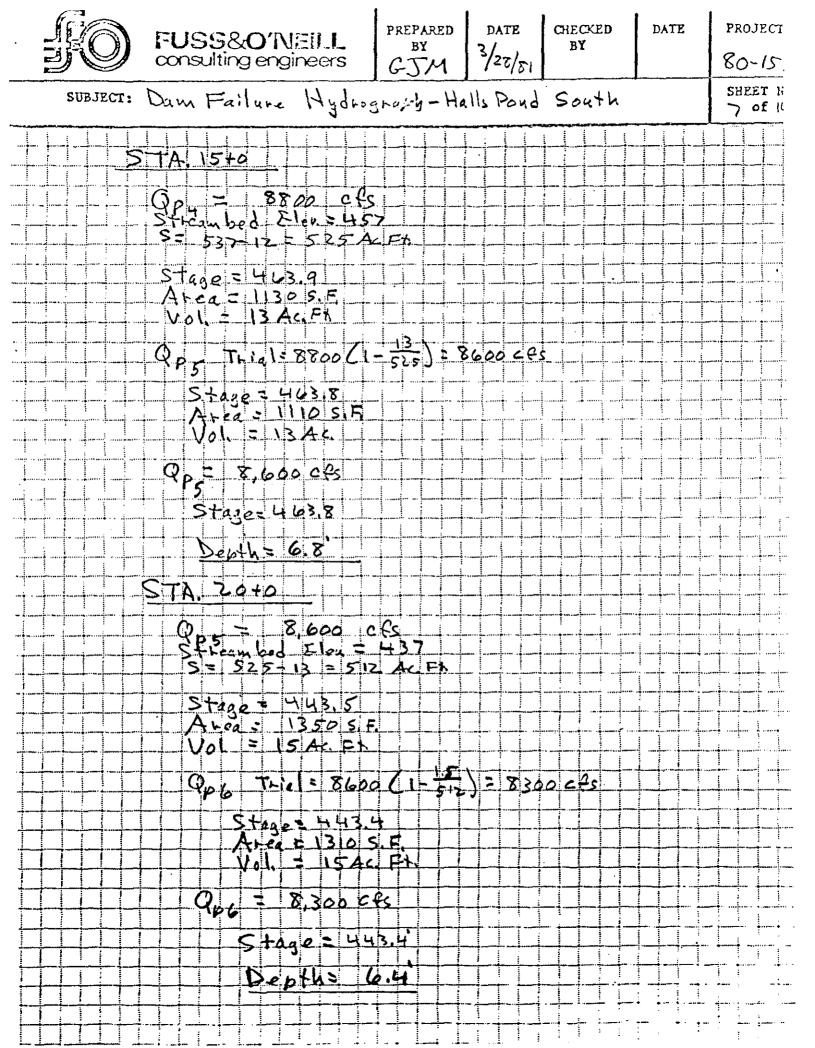
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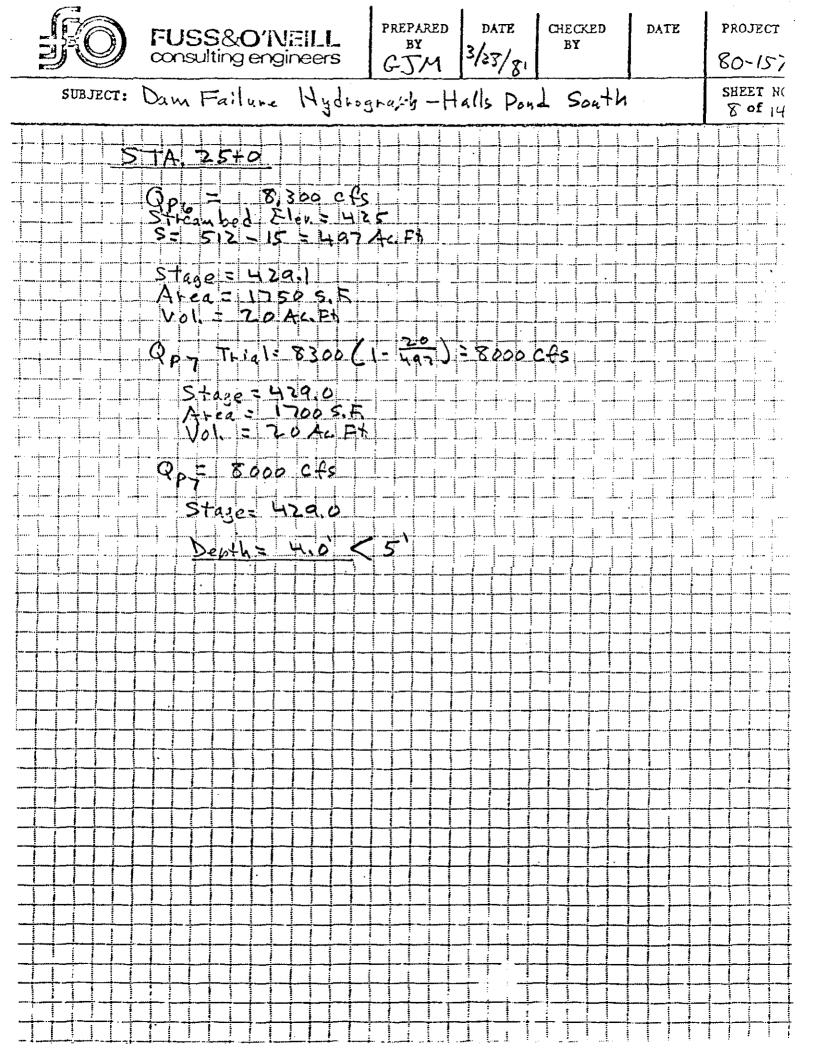
PROJECT : 80:15

SUBJECT: Dam Failure Hudrograph - Halls Pond South

SUBJEC	II: Dam Failure Hydrograph - Halls Poud South	5 of 1
	Storage = SESSO AUFA	
	Top of Dam Elev. = 517.5	<b> </b>
	Riverland Elev. at Sta, 1+0=503.5 & Dam = 0+0	
	Dan Length at M2-Height = 260	
	760x.40 = 104 = Breach W 14h=Wb	
_	<u> </u>	
	Pp = 8/27 V 6 V 3 V 6	
		-
	1 1 3 9, 200 ¢ 85	
	STA-1400	
	5tage= 514.7	
	Area= 1890 S.F.	
	VOUS YACAS	
	Qp2712 = 9200 (1-550) = 9,100 c.8s	
	Stane = 54.7	
	1 ALCa = 1870 S.F.	
	1 VOL = 4 ALPS	
<del>                                     </del>	Rpz = 9,100 cBs	
	<del>                                      </del>	
	5+442 514.7	
	Del712 11.2	
1-1-	<del>                                      </del>	
	<del>╅╌┇╌╏╒╏╒╏╌╏╌╏╌╏╌╏╌╏╌╏</del> ╌╏╌╏╌╏╌┩╌╏╶╃╌╏ <del>╒╿╸╏╸╏╸╏╸╏╸╏╸╏</del>	
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## FUSS&O'NEILL consulting engineers

PREPARED BY GJM DATE 3/30/81 CHECKED BY

DATE

PROJECT NO

SUBJECT: Dam Failure Hydrograph - Halls Pond North

-	<u> </u>	GE - DIS	CHAR	<u>&amp; E</u>		
	5-1-141	SLOPE		F, C) A T/O4	1000	
1	STATION	Score	<u>n</u> _	ELEVATION	AREA	<u> </u>
	0470	375%	.100	505	1930	12,000
<u>-</u>			200	510	3510	28,700
				310		- 20,700
	5+0	5.0%	.100	485	450	3,400
				490	1260	14,400
	10+0	2.6%	.100	465	1750	12,400
				470	3880	36,800
	15+0	0.66%	.100	455	1200	3,900
				460	7880	13,100
				465	5130	29,600
44	20+0	0.66%	.100	450	560	1,200
				455	1920	7,700
				460	3720	20,100
-  -					<u> </u>	
	25+0	0.66%	.100	450	670	2,200
				455	1520	7,400
1-1				460	2560	15,600
1-1-						
T	3010	2.0%	.100	440	350	1700
17				445	1100	7,300
				HSO	23.50	19,700
7						
	3510	6.7%	080	420	450	5,900
				425	1100	19,300
	3740	2.6%	040	410	120	8,00
1				415	860	13,800



PREPARED BY GJM

CHECKED BY DATE

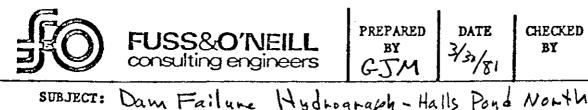
DATE

PROJECT NO 80-157

SHEET NO.

SUBJECT: Nam Failure Hul 11. Halle Dand No. 10

30	"""""	10 of 14
	Storages S = 550 Ac. Ft.	
	Top of Dam Elev. 518.0	
	Riverbed Elev. at Sta, 0+0 (4 Dam = 0+0) = 494.5	
	Dam Length at Mil-Height 185	
	185x40 = 74 = Breach W 2th = Wb	
	Yo = 23.5	
	Rp = 8/27 W6 V g 7 70 3/2	
	# 14,200 cls	
1	STA, 0+70	
	Stage = 505,7	
	Aug = 2140 5,5	
	Vol. = 3 Ac. Ft.	
	902 Th: al = 14,200 (1-550) = 14,100 CES	
	Stage = 505.6	
_		
	Vol = 3 Ac. Pt.	
	Qp= 14,100 cfs	
	Stage = 505.6	
	Depth = U.	
<del>  -</del> -	<del>·</del>	4 4

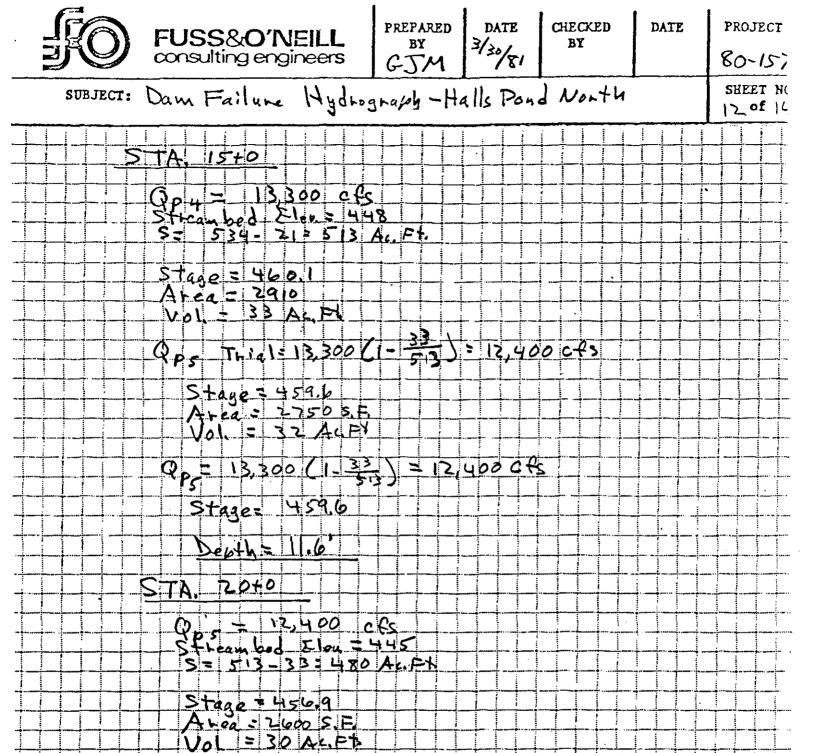


NOLTH SHEET N

DATE

PROJECT

SUBJECT: Dam Failure Hydrograph - Halls Pond North II of It STA 5+0 (302 = 14,100 cfs Strambed Elev = 480 S= 550-3= 547 Ac.Ft Stage = 489.9 Area = 1240 S.F. Vol. = 12 Ac. Ft. Qp3 Thial= 14,100 (1-547)= 13,800 cfs Stage = 489.7 Area = 1220 S.F. VOL = 13Ac Fb Qp3= 14,100 (1-547)=13,800 Stage= 489.7 Deuth = 9.7' STA. JO+0 13,800 cfs Qp3 = 13,800 Cts SFReambod Elou = 456 S= 547-13 = 534 AGFT Stage = 465.3 Avea: 1870 S.F. Vol = 21 A. Ft. Qpy Tral= 13,800 (1-21)= 13,300 CAS Stage 4 465.2 Area # 1830 5.F = 13,300 cfs 5 tage = 465.2 Depths 9.2



The = 12,400 ( - 120) = 1,600 ces

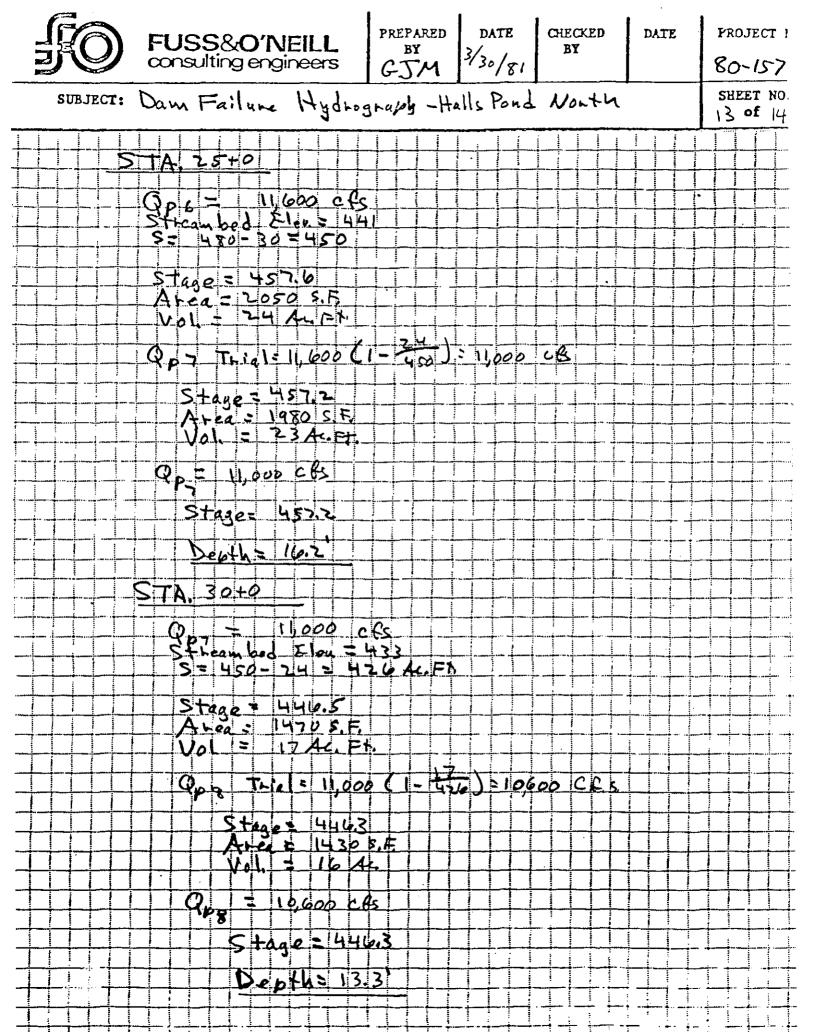
Stage 4 756.6

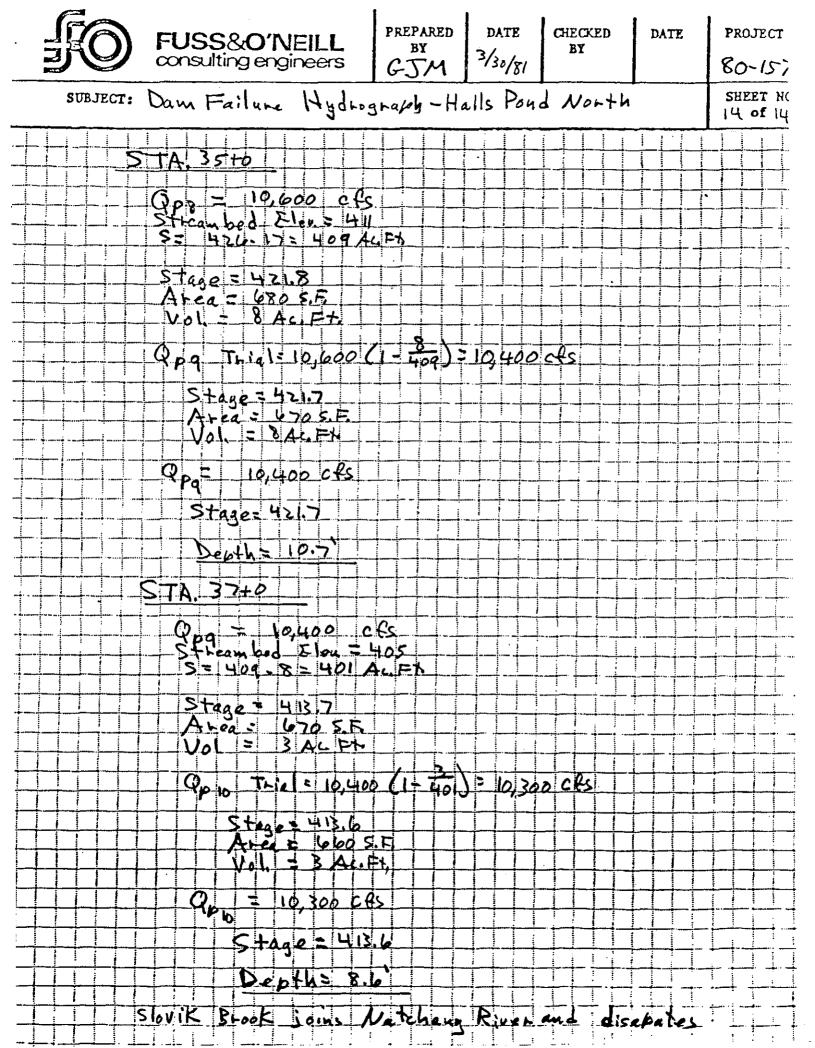
Area E 2490 S.F.

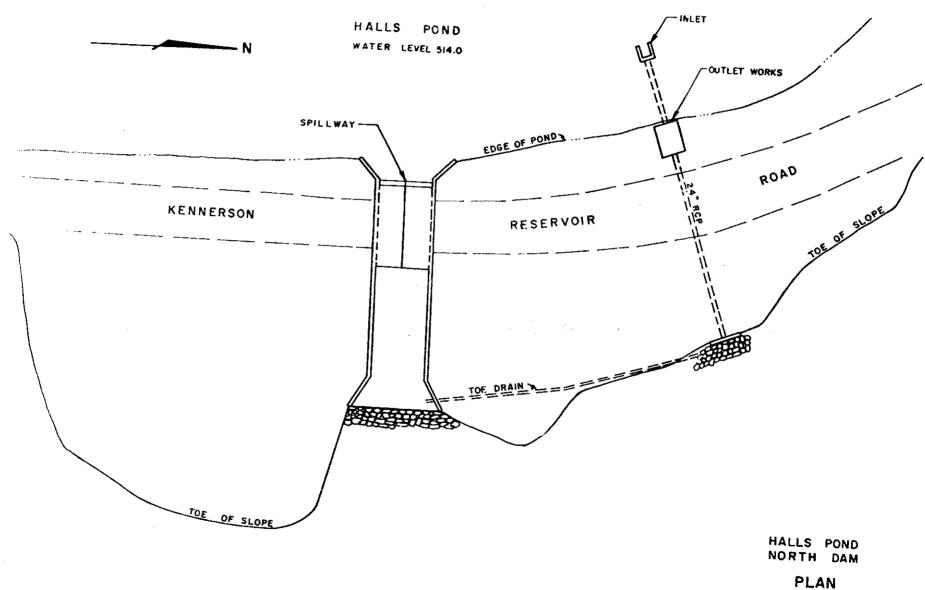
5 tage = 456.6

Depth: 1.6

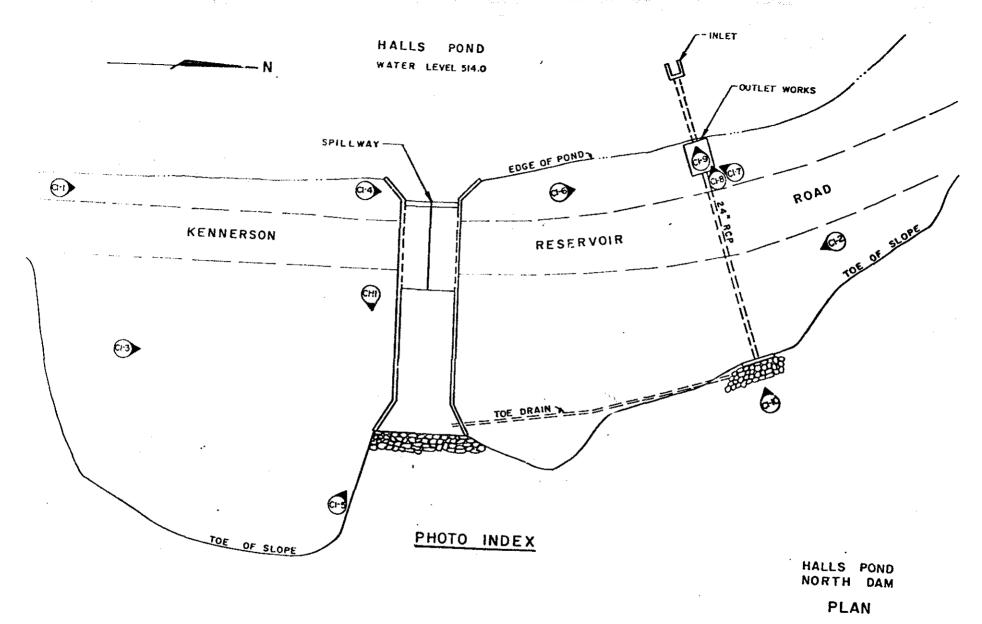
11,600 CES







SCALE (\* 20' PLATE B-1



SCALE [ = 20'

and the committee of the contraction of the contraction of the second of the contraction 
HALLS POND
SOUTH DAM

TYPICAL SECTION

SCALE: 1/4"=1'-0" PLATE B-5